All-Optical Flip-Flop Based on an SOA/DFB-Laser Diode Optical Feedback Scheme

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Abstract—We report on the dynamic all-optical flip-flop (AOFF) operation of an optical feedback scheme consisting of a semiconductor optical amplifier (SOA) and a distributed feedback laser diode (DFB-LD), bidirectionally coupled to each other. The operation of the AOFF relies on the interplay between the optical powers in both the DFB-LD and the SOA. Switching times as low as 150 ps for switch pulse energies of around 6 pJ and a repetition rate of 500 MHz have been measured. The contrast ratio was measured to be above 12 dB.

Index Terms—Optical bistability, optical signal processing, semiconductor optical amplifiers (SOAs).

I. INTRODUCTION

As the network traffic load keeps on increasing, all-optical networks and more in particular packet or burst switched all-optical networks start to become a viable competitor to standard networks employing optical–electronic–optical conversions [1]. In these packet switched optical networks, there is a need for devices such as all-optical flip-flops (AOFFs) that show latching capabilities needed for packet header buffering and routing [2]–[4].

Over time different AOFFs have been proposed such as devices based on multimode interference bistable laser diodes [4], coupled laser diodes [5], or coupled Mach–Zehnder interferometers [6]. The reported switching times of these devices is typically a couple of hundred picosecond, while the length of the set and reset pulses used to switch the device are usually quite long.

Previously we reported static bistable operation of a semiconductor optical amplifier (SOA) bidirectionally coupled to a distributed feedback laser diode (DFB-LD) [7]. In addition to that, dynamic simulations showed that the device can also be used as an AOFF, i.e., can be set and reset using optical pulses [8]. Here we present for the first time experimental results on the dynamic behavior of this new AOFF. Switching times of about 150 ps, switch pulse energies of around 6 pJ, and a repetition rate of 500 MHz were achieved with pulse lengths as low as 150 ps.

The device used here as an AOFF basically consists of a travelling wave SOA which is bidirectionally connected to a laser diode (in this case a DFB-LD) through a coupler. In the actual device, the SOA is connected through a 1 by 4 coupler to four DFB laser diodes of which only one is used and shown here for clarity reasons. The bidirectional coupling causes a certain fraction of the DFB-LD power to be coupled into the SOA while at the same time the same fraction of the SOA output power gets coupled into the DFB-LD. This leads to a strong interaction between the optical fields of the DFB-LD and the SOA.

When a continuous-wave (CW) beam is injected at the SOA side, it has been shown that bistable operation can occur with the actual state depending on the history of the device [7]. The two stable states are defined as either the state where the laser diode is switched ON or the state where the laser diode is switched OFF. It is pointed out that the DFB-LD could also be replaced by another antireflection-coated laser diode, e.g., a tuneable sampled grating-distributed Bragg reflector laser diode.

In the ON-state, the laser light gets partially injected into the SOA causing the SOA to get deeper into saturation and thereby also decreasing the gain for the injected CW signal (and, therefore, also the power injected into the laser diode). When a reset pulse is added to the CW input power to the SOA (Port 1), the output power of the SOA rises and the laser diode can be switched OFF by this additional injected power. Once the pulse has disappeared again, the SOA has a higher gain for the CW signal than in the ON-state and the amplified CW signal can quench the gain in the laser diode forcing it to remain in the OFF-state. To switch back to the ON-state, a set pulse can be injected into the DFB-LD (Port 2), which, after having arrived at the SOA, can decrease the gain there momentarily giving the laser field the time to build up again.

A schematic representation of the device used as an AOFF is shown in Fig. 1. Since the device is based on optical feedback, the device can be used for a broad wavelength range of the CW input signal and set and reset pulses. The only limitation on the wavelength lies in the fact that reflections of the injected signal by the Bragg grating of the DFB laser diode need to be avoided. To that extent, the wavelength of the injected signals need to be sufficiently distant from the Bragg wavelength of the laser diode.
III. EXPERIMENTAL RESULTS

To determine a proper working point for the AOFF, the static response of the device was first investigated. In Fig. 2, the output power of the DFB-LD as a function of the CW input power into the SOA is shown. It can be seen that for a CW input power between 2.4 and 8.4 dBm, the device exhibits bistability with a contrast ratio between the two states of over 35 dB. The CW input power can be lowered by improving the fiber-to-chip coupling in future devices.

For the dynamic experiments, pulses as shown in Fig. 3 were generated using a 40-Gb/s modulator. From this pulse train, the set and reset pulses were obtained by using a 3-dB splitter. Both the set and reset pulses were then separately amplified by an erbium-doped fiber amplifier before being fed to the AOFF. The CW signal wavelength and the pulse wavelength were set at 1555 nm. The wavelength of the DFB-LD was 1538.7 nm. The drive current for the SOA was 103.5 mA and for the DFB-LD 101.4 mA. The output state of the AOFF is determined by the output power of the DFB-LD (after passing through an optical bandpass filter).

AOFF operation using 150-ps-long set and reset pulses with energies of 6.1 and 4.4 pJ, respectively, is shown in Fig. 4. The CW power was 4.4 dBm in this case. A contrast ratio of 12 dB can be observed. Here two set pulses (and also two reset pulses) are defined during each period of 6.4 ns. The first pulse occurs at the beginning of the period while the second one is generated 2 ns later (as can be seen in Fig. 4). The delay between the set and reset pulse was determined by the difference in path length to the front (SOA) and backside (DFB) of the device and was measured to be about 1.2 ns.

Looking in more detail at the actual switching of the device (Fig. 5), we note that a rise time of about 150 ps can be obtained. The relaxation oscillation of the laser diode can be observed as well along the rising edge. The fall time is also measured to be around 150 ps. The rise and fall times of the device suggest that the flip-flop can be turned OFF and ON again in just 300 ps. The shortest realizable ON-OFF-ON cycle may be significantly longer for the flip-flop to remain bistable. The repetition rate measures the actually realized cycle switching rate. Here we report a cycle repetition rate of 500 MHz.

When using 300-ps-long pulses, for the same CW input power, switching between the two states of the AOFF can still be obtained as shown in Fig. 6. In this case, the required switching energies were 5.5 pJ for the set pulse and 7.5 pJ for the reset pulse. Again a repetition rate of 500 MHz between two set or reset pulses can be observed. The contrast ratio is in this case 12.7 dB.

When looking at Fig. 7, one can see that due to the longer pulses both the rise and fall time increase. The rise time is around 200 ps but the fall time increases significantly to about 250 ps. This might be due to the fact that the reset pulse first passes through the SOA, pushing it deeper into saturation, resulting in only a small initial change in the laser power that gets coupled back to the SOA. This small decrease of the laser power in turn causes only a small increase in the gain of the device. The relaxation oscillation of the laser diode can be observed as well along the rising edge. The fall time is also measured to be around 250 ps. The rise and fall times of the device suggest that the flip-flop can be turned OFF and ON again in just 300 ps. The shortest realizable ON-OFF-ON cycle may be significantly longer for the flip-flop to remain bistable. The repetition rate measures the actually realized cycle switching rate. Here we report a cycle repetition rate of 500 MHz.

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SOA. This optical feedback may last as long as the reset pulse is present in the device.

By changing the CW input power to the SOA to 7.4 dBm, it is shown in Fig. 8 that AOFF operation can be maintained over almost the entire range of CW powers for which bistability is obtained. The required pulse energies are in this case 15.8 and 4.3 pJ for the set and reset pulses, respectively. The contrast ratio is now 11.1 dB. The change in pulse energies as compared to the case where the CW input power to the SOA was 4.4 dBm can be explained by looking at Fig. 2. For higher CW input powers, the working point of the device shifts to the right boundary of the bistable domain, implying that less additional power is needed to switch the AOFF from the ON-state to the OFF-state. On the other hand, since the working point moved away from the left boundary of the bistable domain, the power or energy needed to switch the AOFF from the OFF-state to the ON-state will be higher.

Fig. 9 again shows the switch ON and switch OFF response of the AOFF. In the turn-ON response of the AOFF [Fig. 9(a)], the relaxation oscillations of the DFB laser diode are more pronounced then in Fig. 5(a). This is caused by the fact that the higher CW input power (7.4 dBm in stead of 4.4 dBm) quenched the gain of the laser more in this case, giving rise to the increased height of the relaxation oscillations. However, both rise and fall time are again measured to be around 150 ps.

IV. CONCLUSION

AOFF operation of an optical feedback scheme consisting of an SOA and a DFB-LD has been reported. Pulse energies as low as 4.4 and 6.1 pJ for the set and reset pulse, respectively, have been shown. The AOFF shows a contrast ratio of 12 dB and can be operated with a pulse repetition rate of at least 500 MHz. Furthermore, it has been shown that both the CW input power and the pulse length can be varied, but increasing the pulse length also increases the switching time of the device. As the switch ON of the device essentially requires the laser diode to switch ON, the laser diode will impose a lower value to the obtainable switching times but by using short pulses switching times below 100 ps should be possible.

REFERENCES